

Lecture 8.

Summary

1. Maxwell equations

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\vec{D} = \epsilon \vec{E}$$

$$\nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t} + \vec{J}$$

$$\vec{B} = \mu \vec{H}$$

$$\nabla \cdot \vec{D} = \rho_{\text{net}}$$

$$\vec{J} = \sigma \vec{E}$$

$$\nabla \cdot \vec{B} = 0$$

$$\vec{E} \perp \vec{H} \perp \vec{k}$$

2. Plane wave solution

$$\vec{E}_c = \vec{E}_{co} \exp [i(\omega t - \vec{k} \cdot \vec{r})]$$

$$\vec{k} \cdot \vec{k} = \frac{\omega^2}{N^2}$$

$$N = \sqrt{\epsilon_r} = n + ik$$

3. Poynting vector

$$\langle \vec{S} \rangle = \frac{1}{2} \operatorname{Re} (\vec{E}_c \times \vec{H}_c^\perp)$$

4. Boundary conditions

$$\vec{n} \cdot (\vec{D}_1 - \vec{D}_2) = \vec{P}_s$$

$$\vec{n} \cdot (\vec{B}_1 - \vec{B}_2) = 0$$

$$\vec{n} \times (\vec{E}_1 - \vec{E}_2) = 0$$

$$\vec{n} \times (\vec{H}_1 - \vec{H}_2) = \vec{J}_s$$

$$\vec{E}_i = \vec{E}_{i\parallel} \exp[-i\omega(\omega t - \vec{k}_i \cdot \vec{r})]$$

plane wave

$$= \vec{E}_{i\parallel} \exp\{-i[\omega t - k_x i x - k_y j y - k_z z]\} \quad (k_{x_i}^2 + k_{y_i}^2 + k_{z_i}^2 = \frac{\omega^2}{c^2})$$

$$\vec{E}_r = \vec{E}_{r\parallel} \exp\{-i[\omega t - k_{xr} x - k_{yr} y - k_{zr} z]\}$$

$$\vec{E}_t = \vec{E}_{t\parallel} \exp\{-i[\omega t - k_{xt} x - k_{yt} y - k_{zt} z]\}$$

No surface charge, $z=0$

$$E_{i\parallel} \cos\theta_i \exp[+k_{xi} x] + E_{r\parallel} \cos\theta_r \exp[+k_{xr} x] = E_{t\parallel} \exp[i k_{xt} x]$$

$$k_{xi} \sin\theta_i = k_{xr} \sin\theta_r = k_z \sin\theta_t$$

$$\theta_i = \theta_r = \theta_1 \quad | \quad \theta_t = \theta_2$$

$$\frac{\omega}{c_1} \sin\theta_1 = \frac{\omega}{c_2} \sin\theta_2$$

$$n_1 \sin\theta_1 = n_2 \sin\theta_2 \rightarrow \text{Snell law}$$

$$E_{i\parallel} \cos\theta_i + E_{r\parallel} \cos\theta_r = E_{t\parallel} \cos\theta_t \quad (1)$$

$$\nabla \times \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t}$$

$$\left(\begin{array}{ccc} \cancel{E_{r\parallel}} & \hat{i} & \hat{j} & -\hat{k} \\ \cancel{0} & \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ E_{ix} & 0 & E_{iy} \end{array} \right) = -\mu \begin{pmatrix} -i\omega H_{x0} \\ -i\omega H_{y0} \\ -i\omega H_{z0} \end{pmatrix}$$

$$E_{i\parallel} \cos\theta_i \exp[]$$

$$-E_{r\parallel} \sin\theta_r \exp[]$$

$$H_{y0} = \frac{i k E_{\parallel i}}{i \omega \mu} \Rightarrow \vec{H}_{y\perp} = \frac{n_1 E_{\parallel i}^*}{\mu c} \exp\{-i(\omega t - k_x x - k_z z)\}$$

$$\vec{H}_{y\parallel} = -\frac{n_1 E_{\parallel i}}{\mu c} \exp\{-i(\omega t - k_x x + k_z z)\}$$

Continuity of tangential component of $\vec{H} \Rightarrow$

$$n_1 E_{\parallel i} - n_1 E_{\parallel r} = n_2 E_{\parallel s}$$

$$r_{\parallel} = \frac{E_{\parallel r}}{E_{\parallel i}} = \left. \begin{array}{c} -n_2 \cos \theta_i + n_1 \cos \theta_t \\ n_2 \cos \theta_i + n_1 \cos \theta_t \end{array} \right\}$$

$$t_{\parallel} = \left. \begin{array}{c} 2n_1 \cos \theta_i \\ n_2 \cos \theta_i + n_1 \cos \theta_t \end{array} \right\}$$

similarly

r_{\perp}

t_{\perp}

Poynting Vector : $\langle \vec{S} \rangle = \frac{1}{2} \operatorname{Re} \{ \vec{E} \times \vec{H}^* \}$

~~$\langle \vec{S} \rangle = \frac{1}{2} \operatorname{Re} \{ \vec{E} \times \vec{H}^* \}$~~

Reflectivity = $\frac{1}{2} \operatorname{Re} \left\{ \begin{array}{ccc} \hat{i} & \hat{j} & \hat{k} \\ E_x \cos \theta_i \exp(i k_x x) & 0 & -E_{\parallel i} \sin \theta_i \exp(i k_x x) \\ 0 & +\frac{n_1 E_{\parallel i}^*}{\mu c_0} \exp(-i k_x x) & 0 \end{array} \right\}$

$$= \frac{1}{2} \operatorname{Re} \left\{ \frac{n_1 E_{\parallel i}^2 \cos^2 \theta_i}{\mu c_0} \hat{i} + \frac{n_1 E_{\parallel i}^2 \cos \theta_i}{\mu c_0} \hat{k} \right\}$$

Bi-directional reflectance

Reflectivity $R = \left| \frac{E_{\parallel r}}{E_{\parallel i}} \right|^2 = |r|^2$

Transmissivity $T = \frac{S_{z\perp}}{S_{z\parallel}} = \frac{n_2 \cos \theta_z}{n_1 \cos \theta_i} |t|^2 \Rightarrow R + T = 1$

$$k_2^2 = \frac{N_2 \omega}{c_0}$$

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$$\vec{E}_T = \vec{E}_{T1} \exp\{-i\omega t\}$$

$$k_2 \sin \theta_t = k_1 \sin \theta_1$$

$$N_2 \sin \theta_t = n_1 \sin \theta_1$$

$$\text{Or complex. } \sin \theta_t = \frac{e^{i\theta_t} - e^{-i\theta_t}}{2i}$$

$$\cos \theta_t = \frac{e^{i\theta_t} + e^{-i\theta_t}}{2} = a + bi$$

$$\vec{E}_T = \vec{E}_{T1} \exp \left\{ -i(\omega t - \frac{k_1 \sin \theta_1 x - k_2 \cos \theta_1 z}{c_0}) \right\}$$

$$= \vec{E}_{T1} \exp \left\{ -i(\omega t - az) - bz \right\} \\ - k_2 \sin \theta_1 x$$

constant phase plane

$$\omega t - az - k_2 \sin \theta_1 x = 0$$

constant amplitude plane $z = \text{constant} \Rightarrow \text{Inhomogeneous wave}$

Fresnel formula $r_{11} \rightarrow \text{complex}$

$t_{11} \rightarrow \text{complex.}$

But Poynting vector

$$\langle \hat{S} \rangle = \frac{1}{2} \operatorname{Re} \left\{ \frac{N_2 E_{11}^2 \sin^2 \theta_2}{\mu c_0} \hat{i} + \frac{N_2 E_{11}^2 \cos \theta_2}{\mu c_0} \hat{k} \right\}$$

$$R = |r_{11}|^2, T = \frac{\operatorname{Re}(N_2 \cos \theta_1)}{R_1 \cos \theta_1} |t_{11}|^2.$$

Discussion: (1) Critical angle

$$\theta_2 = 90^\circ$$

$$n_1 \sin \theta_{cr} = n_2 \Rightarrow \sin \theta_{cr} = \frac{n_2}{n_1}$$

When $n_1 > n_2$

(2) When $\theta_1 > \theta_{cr}$,

Evanescent wave

$$\vec{E}_t = \vec{E}_{t\parallel} \exp [i(\omega t - k_x t x - k_z t z)]$$

$$\begin{aligned} k_z t &= k_x \cos \theta_2 = \frac{\omega}{c} \sqrt{1 - \sin^2 \theta_2} \\ &= \frac{\omega}{c} \sqrt{1 - \left(\frac{n_1 \sin \theta_1}{n_2}\right)^2} = +i \not{k} \end{aligned}$$

$$\vec{E}_t = \vec{E}_{t\parallel} \exp [-k z]$$

(3) Brewster angle

$$r_{11} = 0 \quad \left\{ \begin{array}{l} n_1 \cos \theta_2 = n_2 \cos \theta_1 \\ n_1 \sin \theta_1 = n_2 \sin \theta_2 \end{array} \right.$$

$$\Rightarrow \tan \theta_1 = \frac{n_2}{n_1} - \text{Brewster angle}$$

only $r_{11} \neq 0$,

(4) If media 2 is absorbing