SOME BASIC CONCEPTS OF ENGINEERING ANALYSIS



46 MINUTES

LECTURE 1 Introduction to the course, objective of lectures

Some basic concepts of engineering analysis, discrete and continuous systems, problem types: steady-state, propagation and eigenvalue problems

Analysis of discrete systems: example analysis of a spring system

Basic solution requirements

Use and explanation of the modern direct stiffness method

Variational formulation

TEXTBOOK: Sections: 3.1 and 3.2.1, 3.2.2, 3.2.3, 3.2.4

Examples: 3.1, 3.2, 3.3, 3.4, 3.5, 3.6, 3.7, 3.8, 3.9, 3.10, 3.11, 3.12, 3.13, 3.14

INTRODUCTION TO LINEAR ANALYSIS OF SOLIDS AND STRUCTURES

- The finite element method is now widely used for analysis of structural engineering problems.
- In civil, aeronautical, mechanical, ocean, mining, nuclear, biomechanical,... engineering
- Since the first applications two decades ago,
 - we now see applications in linear, nonlinear, static and dynamic analysis.
 - various computer programs are available and in significant use

My objective in this set of lectures is:

• to introduce to you finite element methods for the <u>linear</u> analysis of solids and structures.

["linear" meaning infinitesimally small displacements and linear elastic material properties (Hooke's law applies)]

• to consider

- the formulation of the finite element equilibrium equations

- the calculation of finite element matrices
- methods for solution of the governing equations
- computer implementations
- to discuss modern and effective techniques, and their practical usage.

REMARKS

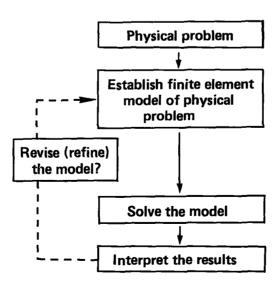
- Emphasis is given to physical explanations rather than mathematical derivations
- Techniques discussed are those employed in the computer programs

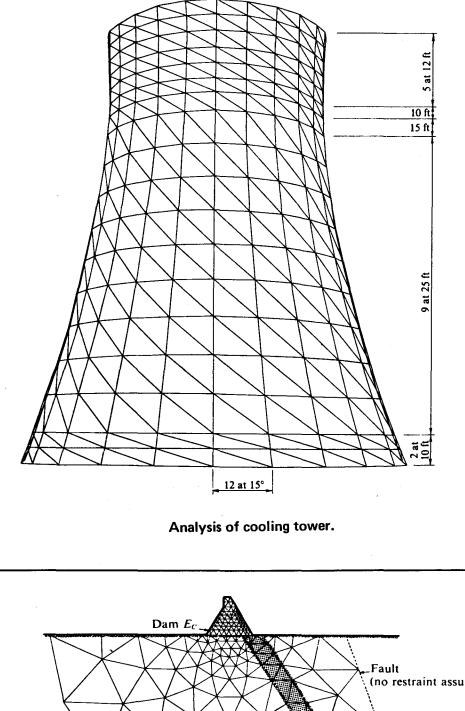
SAP and ADINA

SAP = Structural Analysis Program

- ADINA = Automatic Dynamic Incremental Nonlinear Analysis
- These few lectures represent a very brief and compact introduction to the field of finite element analysis
- We shall follow quite closely certain sections in the book
 - Finite Element Procedures in Engineering Analysis, Prentice-Hall, Inc. (by K.J. Bathe).

Finite Element Solution Process

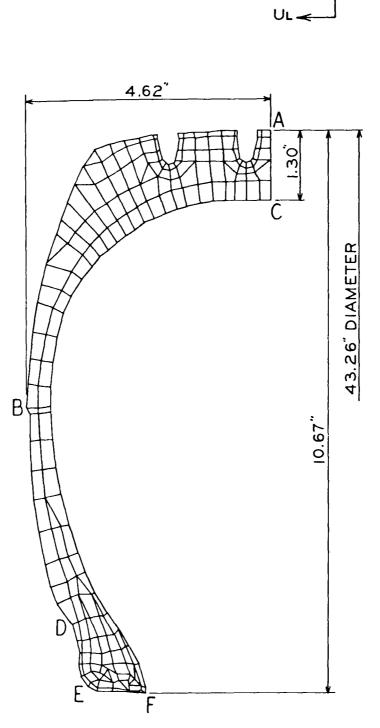




Dam E_c Fault (no restraint assumed) Altered grit $E = \frac{1}{10}E_c$ Mudstone $E = \frac{1}{10}E_c$ Zero displacements assumed

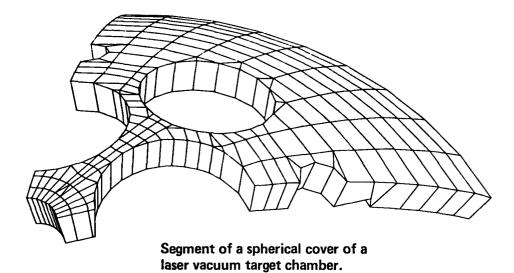
Analysis of dam.

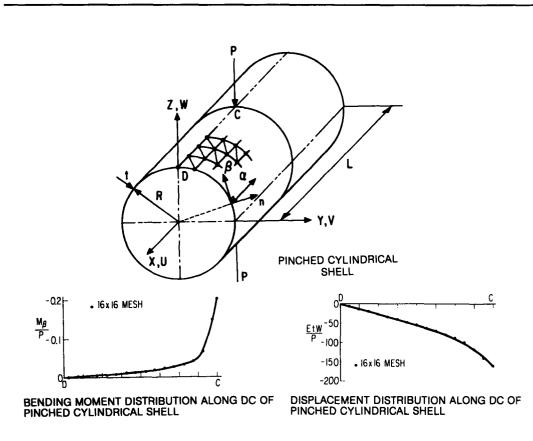
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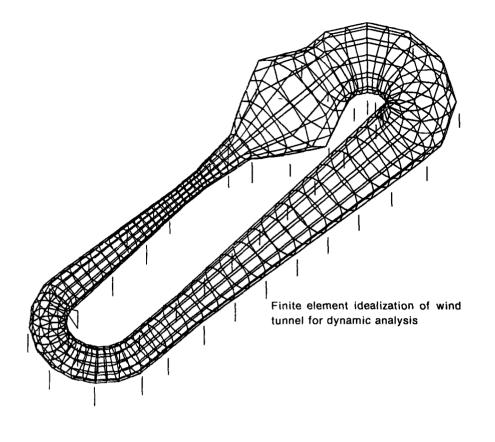


UR

Finite element mesh for tire inflation analysis.







SOME BASIC CONCEPTS OF ENGINEERING ANALYSIS

The analysis of an engineering system requires:

- idealization of system
- formulation of equilibrium equations
- solution of equations
- interpretation of results

SYSTEMS

DISCRETE

CONTINUOUS

response is described by variables at a <u>finite</u> number of points response is described by variables at an <u>infinite</u> number of points

set of <u>alge-</u> braic equations set of <u>differ-</u> ential equations

PROBLEM TYPES ARE

- STEADY-STATE (statics)
- PROPAGATION (dynamics)
- EIGENVALUE

For discrete and continuous systems

Analysis of complex continuous system requires solution of differential equations using numerical procedures

reduction of continuous system to discrete form

powerful mechanism:

the finite element methods, implemented on digital computers

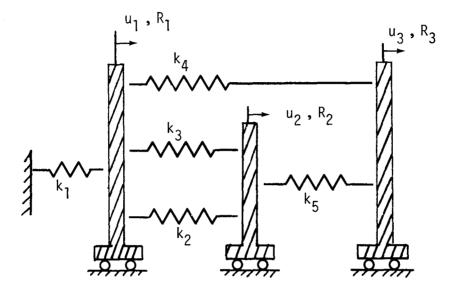
ANALYSIS OF DISCRETE SYSTEMS

Steps involved:

- system idealization into elements
- evaluation of element
 equilibrium requirements
- element assemblage
- solution of response

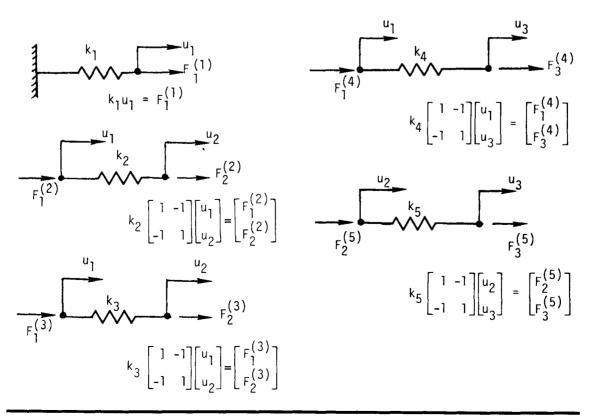
Example:

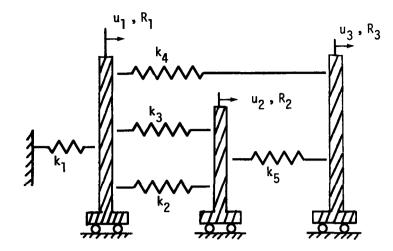
steady – state analysis of system of rigid carts interconnected by springs



Physical layout

ELEMENTS





Element interconnection requirements : $F_1^{(1)} + F_1^{(2)} + F_1^{(3)} + F_1^{(4)} = R_1$ $F_2^{(2)} + F_2^{(3)} + F_2^{(5)} = R_2$ $F_3^{(4)} + F_3^{(5)} = R_3$ These equations can be written in the form

 $\underline{K} \underline{U} = \underline{R}$

Equilibrium equations

$$\underline{K} \ \underline{U} = \underline{R} \quad (a)$$

$$\underline{U}^{T} = \begin{bmatrix} u_{1} & u_{2} & u_{3} \end{bmatrix};$$

$$\underline{R}^{T} = \begin{bmatrix} R_{1} & R_{2} & R_{3} \end{bmatrix}$$

$$\underline{K} = \begin{bmatrix} +k_{4} & & & & \\ k_{1} + k_{2} + k_{3} & -k_{2} - k_{3} & & -k_{4} \\ -k_{2} - k_{3} & & k_{2} + k_{3} + k_{5} & -k_{5} \\ & & & -k_{4} & & -k_{5} & & k_{4} + k_{5} \end{bmatrix}$$

and we note that

$$\underline{K} = \sum_{i=1}^{5} \underline{K}^{(i)}$$

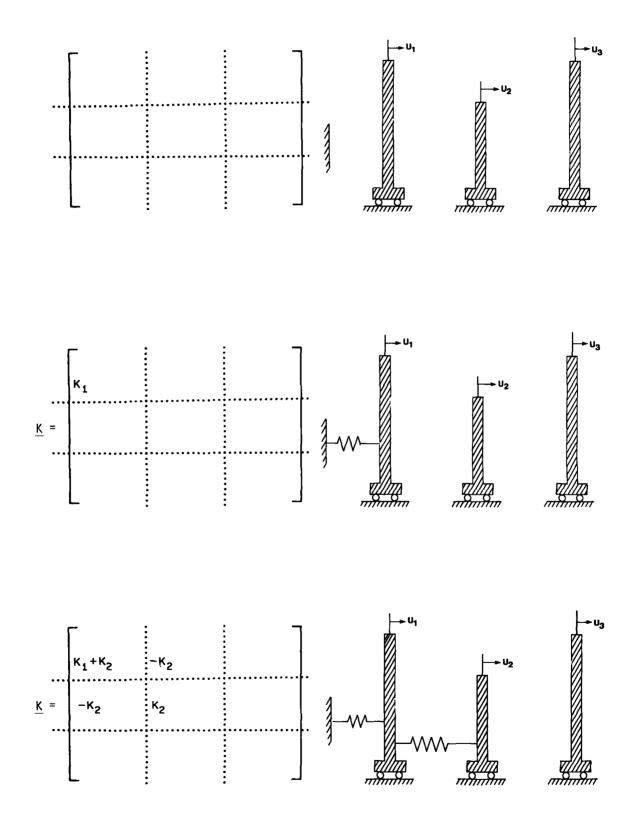
where

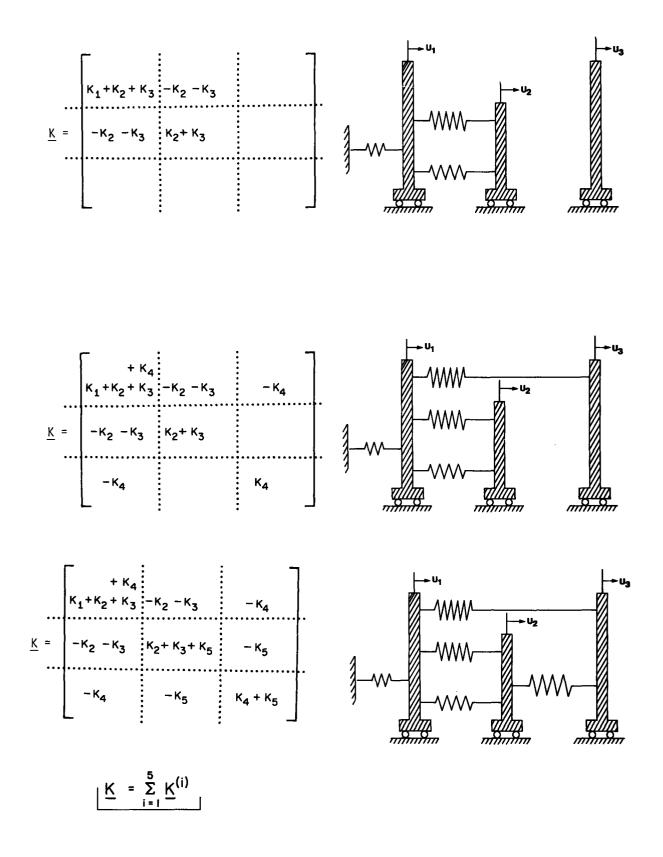
$$\underline{K}^{(1)} = \begin{bmatrix} k_1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$
$$\underline{K}^{(2)} = \begin{bmatrix} k_2 & -k_2 & 0 \\ -k_2 & k_2 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

etc...

This assemblage process is called the <u>direct stiffness</u> <u>method</u>

The steady-state analysis is completed by solving the equations in (a)





In this example we used the <u>direct approach</u>; alternatively we could have used a <u>variational</u> <u>approach</u>.

In the variational approach we operate on an <u>extremum</u> formulation:

 $\Pi = \mathcal{U} - \mathcal{W}$ $\mathcal{U} = \text{strain energy of system}$ $\mathcal{W} = \text{total potential of the loads}$

Equilibrium equations are obtained from

$$\frac{\partial \Pi}{\partial u_i} = 0$$
 (b)

In the above analysis we have

$$\boldsymbol{\mathcal{U}} = \mathbf{\underline{u}}_{2} \underline{\boldsymbol{U}}^{\mathsf{T}} \underline{\boldsymbol{K}} \underline{\boldsymbol{U}}$$
$$\boldsymbol{\mathcal{W}} = \underline{\boldsymbol{U}}^{\mathsf{T}} \underline{\boldsymbol{R}}$$

Invoking (b) we obtain

$$\underline{K} \underline{U} = \underline{R}$$

Note: to obtain $\,\mathcal{U}\,$ and $\,\mathcal{W}\,$ we again add the contributions from all elements

PROPAGATION PROBLEMS

main characteristic: the response changes with time \Rightarrow need to include the d'Alembert forces:

$$\underline{K} \underline{U}(t) = \underline{R}(t) - \underline{M} \underline{\ddot{U}}(t)$$

For the example:

	m	0	0 7
<u>M</u> =	0	^m 2	0
	0_0	0	^m 3 –

EIGENVALUE PROBLEMS

we are concerned with the generalized eigenvalue problem (EVP)

 $\underline{A} \underline{v} = \lambda \underline{B} \underline{v}$

 \underline{A} , \underline{B} are symmetric matrices of order n

- v is a vector of order n
- λ is a scalar

EVPs arise in dynamic and buckling analysis

Example: system of rigid carts

$$\underline{\mathsf{M}} \ \underline{\mathsf{U}} + \underline{\mathsf{K}} \ \underline{\mathsf{U}} = \underline{\mathsf{O}}$$

Let

$$\underline{U} = \underline{\phi} \sin \omega (t-\tau)$$

Then we obtain

$$-\omega^{2} \underline{M} \underline{\phi} \sin \omega(t-\tau) + \underline{K} \underline{\phi} \sin \omega(t-\tau) = \underline{0}$$

Hence we obtain the equation

$$\underline{K} \underline{\phi} = \omega^2 \underline{M} \underline{\phi}$$

There are 3 solutions

$$\begin{array}{c} \begin{array}{c} \omega_{1} , \underline{\phi}_{1} \\ \alpha_{2} , \underline{\phi}_{2} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \omega_{3} , \underline{\phi}_{3} \end{array} \end{array} eigenpairs$$

In general we have n solutions

MIT OpenCourseWare http://ocw.mit.edu

Resource: Finite Element Procedures for Solids and Structures Klaus-Jürgen Bathe

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